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# Kinematic viscosity prediction for aqueous solutions with various solutes

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### **Abstract**

In numerous research areas knowledge of aqueous solutions viscosity is very important to interpret the experimental data or to use it in simulation studies. When Kumar's semitheoretical equation for prediction of the dynamic viscosity of a solution of a single electrolyte is modified for prediction of kinematic viscosities, it is found that the resulting expression is valid both for salts and for certain organic solutes. The parameters characterizing individual solutes in aqueous solution at temperatures between 293.1 and 323.1 K also allow prediction of the kinematic viscosities of solutions of multiple solutes in the same temperature and concentration range, with overall errors of <2.5% in 36 of 39 multi-component systems. © 2001 Elsevier Science B.V. All rights reserved.

*Keywords:* Kinematic viscosity; Aqueous solutions; Electrolytes; Multi-solute solutions

# **1. Introduction**

In numerous research areas, aqueous salt solutions are used as microbiological nutrients [1] or to control chemical properties [2], chemical reaction rates [3] or hydrodynamic characteristics [4]. The studies of gas–liquid mass transfer are frequently facilitated by using aqueous buffer solutions so as to be able to work at constant pH and hence simplify mathematical modeling of the results [5], and the main factors governing the complex mechanism of the absorption processes can be controlled by the addition of salts [6]. In most cases, the salt or salts modify the viscosity of the solvent, which must be taken into account when interpreting experimental data in terms of models involving viscosity directly or via its influence on other properties [7], or when such models are used for simulation studies of industrial processes.

To this end, and to avoid extensive viscosity measurements, and time-consuming literature searches, numerous equations have been developed for prediction of viscosities [8–10]. However, most such equations employ great number of solute-specific parameters, and are of very limited validity for multi-component solutions. One of the simplest is Kumar's expression [10] for relative dynamic viscosity as a function of mole fraction of solute. However, a parameter of more immediate interest in many situations is the kinematic viscosity, which is directly involved in many dimensionless numbers used in chemical engineering in relation to mass transfer processes.

In this work, we re-formulated Kumar's equation as an expression for relative kinematic viscosity in terms of relative density, mass fraction and temperature, and for aqueous solutions of each of 24 common saline or organic solutes determined the parameters minimizing the error in kinematic viscosity. For each solute employed, optimization was based on published data for kinematic viscosities of solutions of various concentrations and temperatures in the range 293.1–323.1 K. Finally, we investigated the accuracy with which the parameters obtained for the individual solutes allowed prediction of the published viscosities of 24 two-solute solutions and 15 three-solute solutions, with excellent results.

# **2. Fundamentals**

Kumar's model [10] for the prediction of the dynamic viscosity  $\mu$  of a solution with a single-solute is

$$
\frac{\mu}{\mu_0} = \frac{1 + bx}{1 - hx} \tag{1}
$$

where  $\mu_0$  is the dynamic viscosity of the solvent, x the mole fraction of solute, and *b* and *h* are parameters whose dependence on temperature *T* is given by polynomials in (*T*−*T*ref) with coefficients that depend only on the solute and solvent when the influence of pressure as negligible:

$$
b = b_{\text{ref}} + \sum_{n} b_n (T - T_{\text{ref}})^n
$$
 (2)

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#### **Nomenclature**



$$
h = h_{\text{ref}} + \sum_{m} h_m (T - T_{\text{ref}})^m
$$
\n(3)

where  $b_{\text{ref}}$  and  $h_{\text{ref}}$  are the values of *b* and *h* at the reference temperature *T*ref, and the degrees of the polynomials, *n* and *m*, are set in the light of the desired accuracy and the number of data available. The parameters *b* and *h* are, respectively, interpreted as a coefficient of solute–solvent interaction and as the number of solvent molecules solvating each solute molecule.

Eq. (1) may be rewritten in the form:

$$
\nu_{\rm rel} = \frac{1}{\rho_{\rm rel}} \left[ \frac{1 + Bw}{1 - Hw} \right] \tag{4}
$$

where *w* is the mass fraction of solute,  $v_{rel}$  and  $\rho_{rel}$  are the ratios between the kinematic viscosities and densities of the

solution and the pure solvent, and *B* and *H* are given by

$$
B = B_{\text{ref}} \sum_{n} B_n (T - T_{\text{ref}})^n \tag{5}
$$

$$
H = H_{\text{ref}} \sum_{m} H_m (T - T_{\text{ref}})^m
$$
\n(6)

(if all the above equations were exact, then *B* and *H* would be related to *b* and *h* via the expression relating mole fraction and mass fraction, i.e. for single-solute solutions,  $x = wM_0/(M - wM + wM_0)$ , where *M* and  $M_0$  are the molecular mass of the solute and solvent)

To parameterize Eq. (4) for solutions of single common solutes in water, we treated the influence of pressure as negligible under normal laboratory conditions (0.1 MPa), and used the Nelder–Mead method [11,12] to optimize the *B* and  $H$  of Eqs. (5) and (6) so as to minimize the deviation between the published data for the kinematic viscosities of solutions of the solute in question and the calculated values given by Eqs.  $(4)$ – $(6)$ , with the aid of the following expressions for the temperature dependence of the density,  $\rho_w$ , and kinematic viscosity,  $v_w$ , of water

$$
\rho_{\rm w} = \rho_{\rm ref} + \sum_{i} \rho_i (T - T_{\rm ref})^i \tag{7}
$$

$$
\nu_{\rm w} = \nu_{\rm ref} + \sum_{j} \nu_i (T - T_{\rm ref})^j \tag{8}
$$

where the parameters  $\rho_i$  and  $v_j$  of Eqs. (7) and (8) having previously been optimized by fitting these equations to published data [13] for the temperature range 293.1–323.1 K.

Independently, Eq. (7) (with the parameters optimized as above) was used together with the published density data for the same solutions as above to optimize the parameters  $d_1$  and  $d_2$  of the expression:

$$
\rho_{\rm rel} = 1 + d_1 w + d_2 w (T - T_{\rm ref}) \tag{9}
$$

In dealing with solutions with more than one solute, the  $d_1w$ ,  $d_2w$ , *bw* and *hw* of the individual solutes were assumed to be additive. Accordingly, the kinematic viscosities of *k*-solute solutions were predicted using the equation

$$
v_{\text{rel}} = \frac{1}{\rho_{\text{rel}}} \left( 1 + \frac{\sum_{k} b_{k} w_{k}}{1 - \sum_{k} h_{k} w_{k}} \right) \tag{10}
$$

where

$$
\rho_{\text{rel}} = 1 + \sum_{k} d_{1k} w_k + (T - T_{\text{ref}}) \sum_{k} d_{2k} w_k \tag{11}
$$

# **3. Results**

In all cases, the reference temperature was 298.1 K. Fitting Eqs. (7) and (8) to the published data for the density and kinematic viscosity of water [13] afforded the parameters listed in Table 1. With these parameters, none of the

Table 1 Parameters of Eqs. (7) and (8) for the density and kinematic viscosity of water at temperatures between 293.1 and 323.1 K

$\rho_{ref}$ (kg/m <sup>3</sup> )	$\rho_1$ (kg/K m <sup>3</sup> )	$\rho_2 \times 10^2$ (kg/K <sup>2</sup> m <sup>3</sup> )	$v_{\text{ref}} \times 10^6 \text{ (m}^2/\text{s)}$	$v_1 \times 10^8$ (m <sup>2</sup> /K s)	$v_2 \times 10^{10}$ (m <sup>2</sup> /K <sup>2</sup> s)	$v_3 \times 10^{12}$ (m <sup>2</sup> /K <sup>3</sup> s)
997.07	$-0.260$	$-4.030$	0.893	$-2.019$	3.596	$-3.822$

values calculated using Eqs. (7) and (8) differed from the corresponding published value by more than 0.05%.

For 20 common salts, in Table 2 are the optimized values of the parameters of the Eqs. (5), (6) and (9), together with the number of data used, *N*, the ranges of mass fraction and temperature covered by these data, and the value of  $\sigma = [\Sigma(\sigma_{\text{cal}} - \sigma_{\text{exp}})^2/(N-I)]^{1/2}$  for the standard deviation between the published [13–19] and the calculated values of the kinematic viscosity, which was  $\langle 1\% \rangle$  in all cases in spite of data from more than one source having been pooled for several of the salts considered. As example, Fig. 1 illustrates the fit achieved for NaCl,  $KNO_3$  and Na<sub>2</sub>CO<sub>3</sub> at 293.1 K, and Fig. 2 illustrates the validity of the assumption of linear dependence of  $\rho_{rel}$  on *w*, Eq. (9).

For most solutes *B* increases and *H* decreases with increasing temperature, but there are exceptions, see Figs. 3 and 4. For a given anion, the values of  $B_{\text{ref}}$  and  $H_{\text{ref}}$  for the sodium salt are in all cases greater than the corresponding value for the potassium salt; and for a given cation and anion family,  $B_{\text{ref}}$  and  $H_{\text{ref}}$  increase with the charge  $q$  of the anion (Fig. 5 shows the behavior of *B*ref in phosphates and carbonates). These trends, like similar trends in the parameters  $b_{\text{ref}}$  and  $h_{\text{ref}}$  of Kumar's equation, appear to be mediated by the radius of the cation, the oxidation state of the anion, the number of ions that the electrolyte is capable of forming, and the adiabatic compressibility [10,20].



Fig. 1. Bibliographic and calculated values of the kinematic viscosity of aqueous Na<sub>2</sub>CO<sub>3</sub>, NaCl and KNO<sub>3</sub> solutions at 293.1 K.

Table 3 shows that equally good fit was obtained for the four organic solutes for which kinematic viscosity data were published [16]. It is worth noting that all four organic solutes have very similar  $B_{\text{ref}}$  values and, except for glycerin, very similar *H*ref values. This is attributable to the structures of all

Table 2

Parameters of Eqs. (5), (6) and (9) for calculation of the densities and kinematic viscosities of aqueous salt solutions

Solute	$w \times 10^2$	T(K)	$d_1$	$d_2 \times 10^3$ (1/K)	$B_{\text{ref}}$	$B_1 \times 10^2$ (1/K)	$B_2\times 10^4$ $(1/K^2)$	$H_{\rm ref}$	$H_1 \times 10^2$ (1/K)	$H_2\times10^4$ $(1/K^2)$	N	$\sigma \times 10^6$ $(m^2/s)$
Na <sub>2</sub> CO <sub>3</sub>	< 14.0	$293.1 - 323.1$	1.010	1.768	4.954	1.397	1.860	3.396	$-2.994$	$-1.762$	50	0.007
$K_2CO_3$	$\leq$ 17.9	293.1-323.1	0.908	$-6.178$	2.154	1.077	0.061	2.039	$-0.311$	$-3.682$	50	0.005
NaHCO <sub>3</sub>	$\leq 8.0$	293.1-323.1	0.696	$-2.846$	2.726	$-0.509$	$-1.087$	2.028	0.423	6.445	30	0.003
KHCO <sub>3</sub>	$\leq$ 13.8	293.1-323.1	0.686	2.942	1.259	1.953	0.728	1.584	$-3.118$	1.376	50	0.003
Na <sub>3</sub> PO <sub>4</sub>	$\leq 7.6$	293.1-323.1	1.225	2.383	5.608	$-1.459$	0.955	4.306	0.712	$-5.994$	35	0.003
$K_3PO_4$	$\leq 20.9$	293.1-323.1	1.109	$-5.500$	2.851	0.080	$-0.010$	2.287	$-0.253$	$-0.886$	42	0.004
Na <sub>2</sub> HPO <sub>4</sub>	$\leq 6.8$	293.1-323.1	1.010	3.506	4.250	1.276	$-8.321$	3.319	0.564	0.071	35	0.003
K <sub>2</sub> HPO <sub>4</sub>	$\leq$ 18.1	$293.1 - 323.1$	0.916	9.784	2.449	2.205	$-2.497$	1.878	$-1.127$	2.919	42	0.003
NaH <sub>2</sub> PO <sub>4</sub>	$\leq$ 13.1	293.1-323.1	0.775	1.559	3.317	1.297	$-3.547$	2.161	$-3.860$	7.514	42	0.004
$KH_2PO_4$	<14.7	$293.1 - 323.1$	0.757	0.337	2.164	1.429	$-5.163$	1.753	$-2.959$	11.83	42	0.002
CuSO <sub>4</sub>	$\leq$ 14.0	293.1-323.1	1.138	8.878	3.912	1.015	$-2.027$	2.756	$-1.809$	2.529	30	0.008
$Fe2(SO4)3$	$\leq 24.0$	293.1-323.1	1.015	22.50	3.759	$-0.448$	1.928	2.632	$-0.727$	0.431	30	0.008
NaCl	$\leq$ 11.0	293.1-298.1	0.741	$-0.461$	1.532	0.545	$-11.49$	1.950	$-0.919$	11.89	20	0.008
KCl	$\leq 13.0$	293.1-298.1	0.692	7.809	0.084	0.280		1.148	7.930	$-14.71$	10	0.006
Na <sub>2</sub> SO <sub>4</sub>	$\leq 13.0$	293.1-298.1	0.956	7.148	3.459	$-2.462$	1.682	2.065	0.984	$-1.017$	10	0.009
K <sub>2</sub> SO <sub>4</sub>	$\leq 10.0$	293.1-298.1	0.887	13.24	1.345	0.079	0.206	1.408	6.443	$-13.53$	10	0.008
NaNO <sub>3</sub>	$\leq$ 14.4	293.1-298.1	0.748	11.11	0.742	2.069	$-6.185$	2.004	$-1.503$	8.189	10	0.009
KNO <sub>3</sub>	$\leq 17.0$	293.1-298.1	0.630	$-3.817$	$-0.235$	1.992	$-0.890$	0.261	$-0.049$	0.971	10	0.009
NaBr	< 10.0	293.1-298.1	0.827	0.381	0.467	2.710	$-3.914$	0.992	$-1.302$	3.128	10	0.005
KBr	$\leq 11.0$	293.1-298.1	0.729	$-6.455$	$-0.215$	2.397	$-3.810$	$-0.057$	$-0.272$	3.904	10	0.005



Fig. 2. Bibliographic and calculated values of the relative density of aqueous Na<sub>2</sub>CO<sub>3</sub>, NaCl, CuSO<sub>4</sub> and KNO<sub>3</sub> solutions at the indicated temperatures.



# *3.1. Kinematic viscosity prediction for aqueous two- and three-solute solutions*

Application of Eq. (11) to the multi-solute systems listed in Table 4 using the single-solute values of  $d_1$  and  $d_2$  listed in Tables 2 and 3 allowed prediction of measured densities to within 1.5% in all cases.

Similarly, for concentrations and temperatures in the ranges considered for the individual solutes, the kinematic



Fig. 3. Temperature dependence of *B* and *H*, Eqs. (5) and (6) for several potassium salts.



Fig. 4. Temperature dependence of *B* and *H*, Eqs. (5) and (6) for several sodium salts.

viscosities calculated from Eq. (10) agree very well with the experimental data published [15–19,22–24], with  $\sigma$  values  $\leq$  0.034 in all cases and  $\leq$  0.022 in all but two (see Table 4); most of this error in fact appears to be attributable to the error in the calculated relative densities.

Note that since Eq. (10) distinguishes the separate contributions of the various solutes to the kinematic viscosity, the dependence of the latter on the mass fraction of each solute can be plotted separately; this is illustrated in Fig. 6 for binary solutions of NaCl, KCl or  $NaNO<sub>3</sub>$  with a fixed concentration of  $Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>$ , and in Fig. 7 for ternary solutions of KCl,  $NaNO<sub>3</sub>$  or  $Na<sub>2</sub>SO<sub>4</sub>$  with fixed concentrations of  $Na<sub>2</sub>CO<sub>3</sub>$  and NaHCO<sub>3</sub>.



Fig. 5. Dependence of  $B_{\text{ref}}$  on the charge of the anion in homologous series of salts.





Table 4

Discrepancy between experimental kinematic viscosities of multi-solute aqueous solutions and those calculated from Eq. (10)





Fig. 6. Bibliographic and calculated values of the kinematic viscosity of binary aqueous solutions of  $Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>$  0.125 kmol/m<sup>3</sup> and various concentrations of NaNO3, NaCl or KCl at 293.1 K.



Fig. 7. Bibliographic and calculated values of the kinematic viscosity of ternary aqueous solutions of Na<sub>2</sub>CO<sub>3</sub> and NaHCO<sub>3</sub>, 0.5 kmol/m<sup>3</sup> each, and various concentrations of NaNO<sub>3</sub>, Na<sub>2</sub>SO<sub>4</sub> or KCl at 293.1 K.

## **4. Conclusions**

At temperatures between 293.1 and 323.1 K, the method proposed in this work allows the kinematic viscosities of aqueous solutions of salts and certain organic solutes to be calculated over a wide range of concentrations from their mass fractions and temperatures, by means of parameters obtained in the same way. The same parameters can be used to additive manner to calculate the kinematic viscosities of multi-solute solutions. These results should facilitate both the processing of data obtained in studies of gas–liquid mass transfer and the simulation of gas–liquid mass transfer processes, because all the solutes considered in this work are commonly employed in such studies.

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